

Design of piezoelectric cantilevers

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MAE 656: Advanced computer
aided design

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Presentation

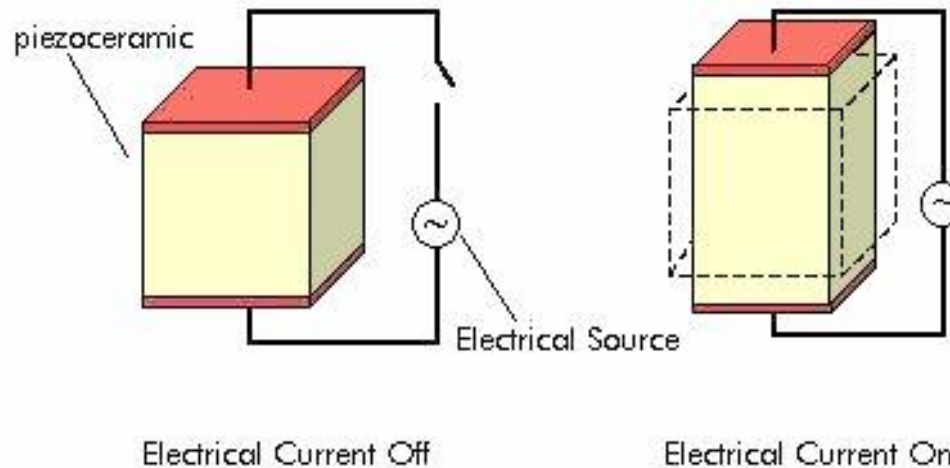
- ❖ Description of the problem solved
- ❖ Description of the numerical model
- ❖ Results obtained with the numerical model
- ❖ Conclusions and summary



Description of the problem solved

Description of the problem solved

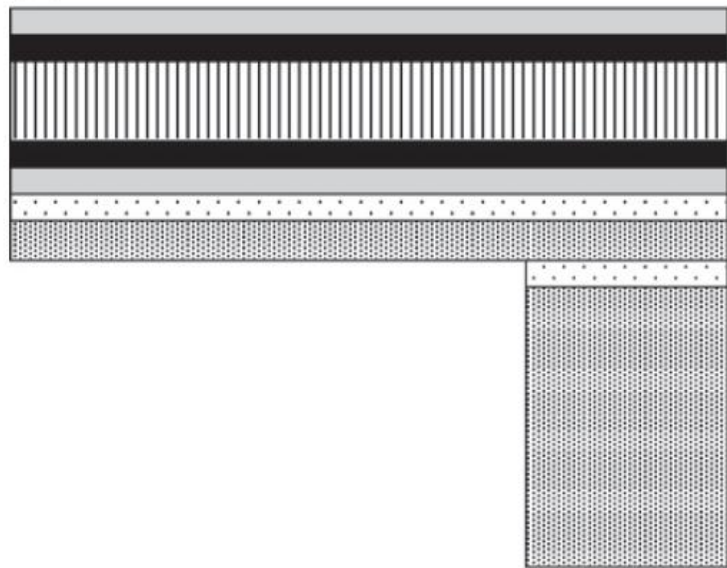
❖ Piezoelectric materials:



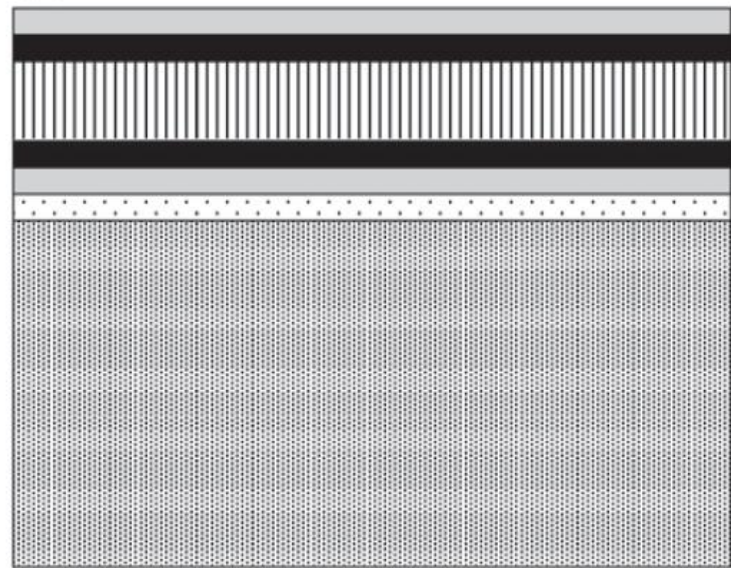
Description of the problem solved

❖ Piezoelectric cantilevers:

(a) Cantilever



(b) Si wafer



Pt



LNO



PZT



SiO₂



Si

[5]

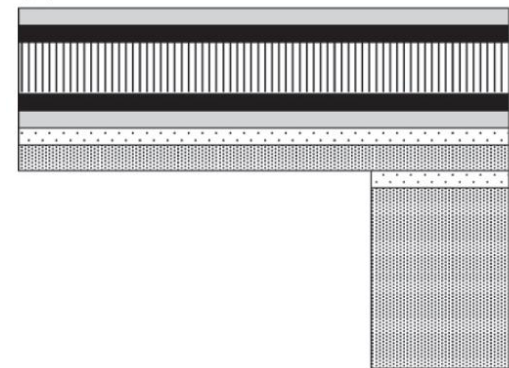
Description of the problem solved

❖ Applications for this cantilevers:

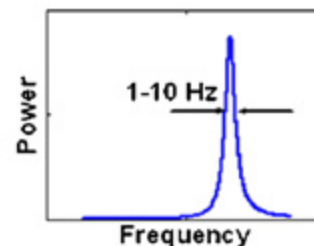
- Accelerometers [1].
- AFM cantilevers [2].
- Harvesters [3].

❖ In all these applications the mechanical resonance frequency is a key parameter.

(a) Cantilever



[5]



Description of the problem solved

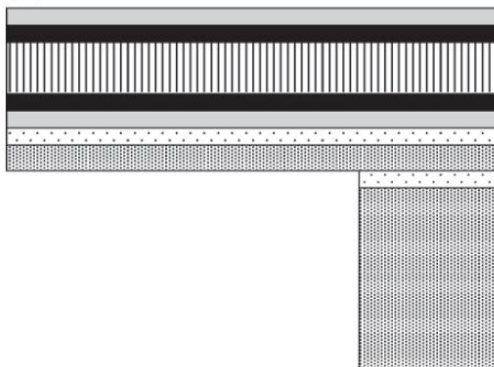
- ❖ The goal of this project is to develop a design criterion.
 - Evaluate the change in stresses when the length and the width is changed.
 - Advantage: the resonance frequency can be tuned without increasing the internal loads.

Description of the problem solved

❖ Fabrication of the cantilever:

- The thickness of the films is defined by the process.

(a) Cantilever



[5]

Material	Thickness (nm)
Pt	175
LNO	115
PZT	960
LNO	200
Pt/Ti	175/5
SiO ₂	540

Description of the problem solved

❖ Fabrication of the cantilever:



(a) Oxidation (3000Å)



(b) Ti (400 Å)/Pt (3500Å)



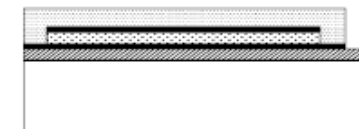
(c) PZT (4500Å)



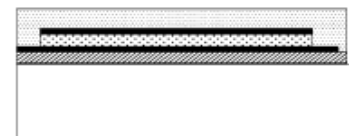
(d) Pt (2000Å)



(e) Dry etching of upper electrode Pt and PZT after photo-resist patterning



(f) Dry etching of lower electrode Pt after photo-resist patterning



(g) SiO₂ dry etching after photo-resist patterning

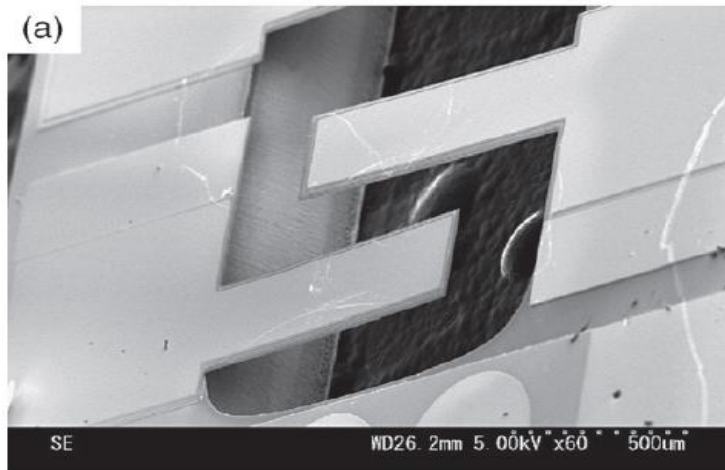


(h) Silicon dry etching by XeF₂ and photo-resist remove

[6]

Description of the problem solved

- ❖ In this project the cantilever made by Kobayashi et.al. [5] will be modeled to know what are the stresses that the materials can support without breaking.



Cantilever dimensions:
270x1000 μ m

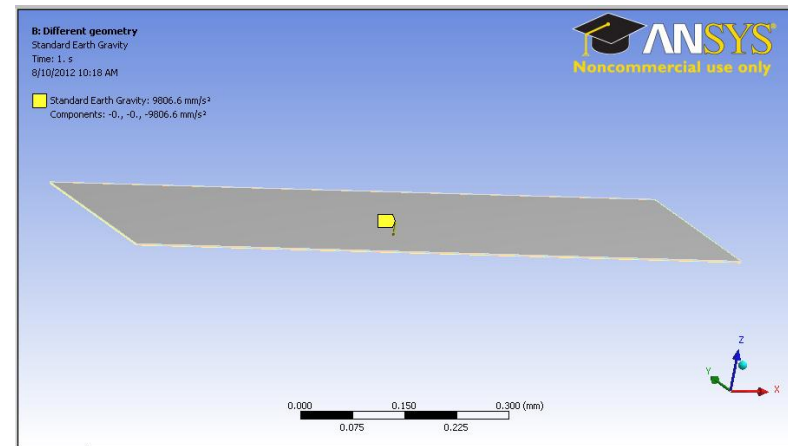
[5]



Description of the numerical model

Description of the numerical model

- ❖ Loads over the cantilever:
 - Gravitational.
 - Process loads*.
 - Loads during the application*.

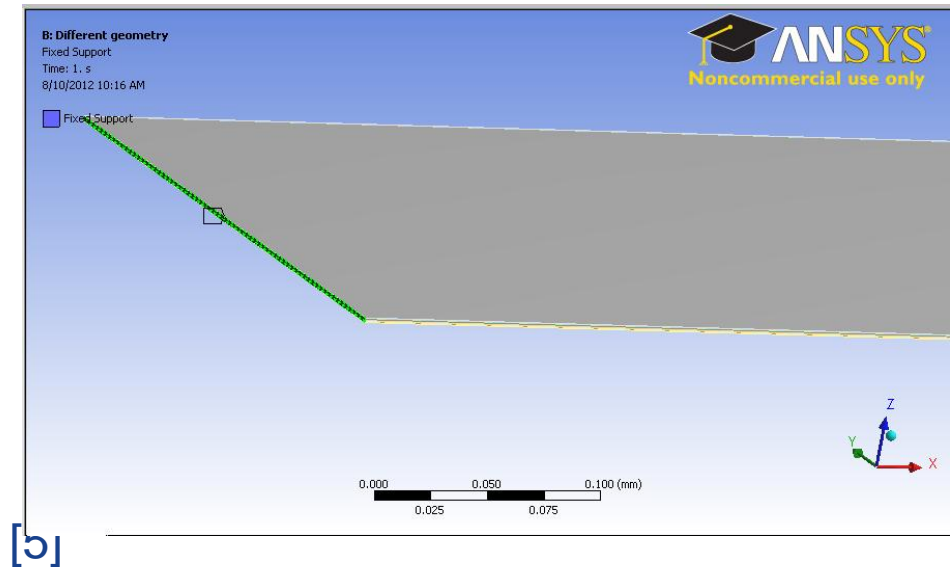
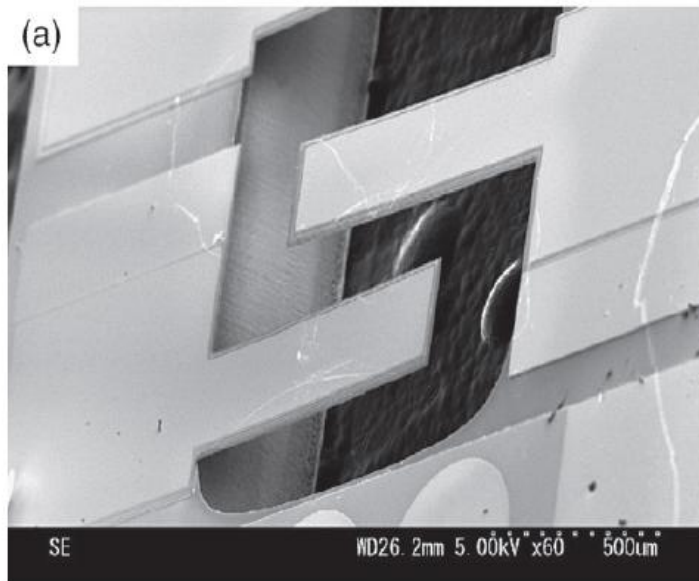


*: not considered in this work

Description of the numerical model

❖ Support:

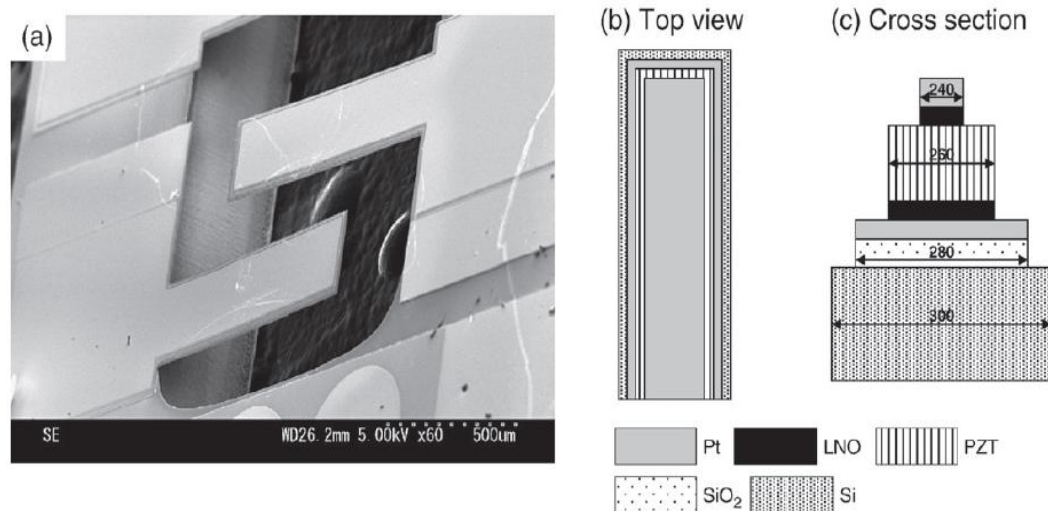
- The cantilever will be supported in the lateral faces.



Description of the numerical model

❖ Geometry approximation:

- Only one width and length will be used for all the layers.
- The Ti layer (5nm) won't be modeled because it is an adhesion layer.



[5]

Description of the numerical model

❖ 3D Modeling:

- In this case we are in the limit where 3D modeling can be used because the smallest lamina dimensions are $1000 \times 270 \times 0.1 \mu\text{m}$.

Description of the numerical model

❖ Materials properties:

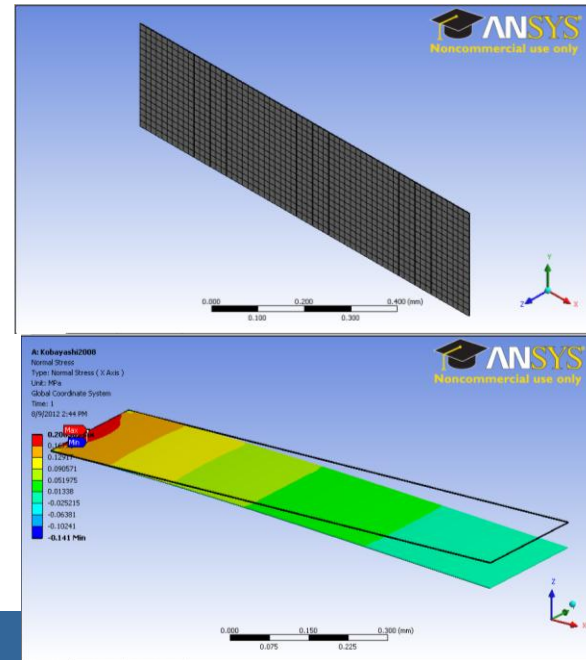
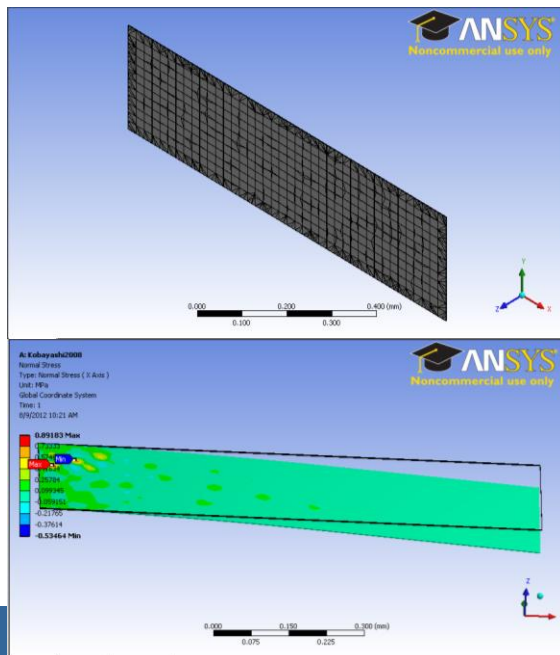
	Density (g/cm ³)	Elastic Modulus (Gpa)	Poisson's ratio	Ref.
SiO₂	2.2	69	0.17	[7]
Pt	21.44	164.6	0.396	[8]
LNO	4.8	69*	0.17*	[9]
PZT	7.6	101	0.3	[10]

*the properties of LNO couldn't be found and they were replaced for the SiO₂ properties.

Description of the numerical model

❖ Meshing:

- First the automatic meshing.
- Secondly, mapping and face sizing.



Description of the numerical model

❖ Meshing:

- Convergence study: problem with the aspect ratio of the elements (Thickness: $0.1\mu\text{m}$). e.g. $16\times 16\times 0.1\mu\text{m}$

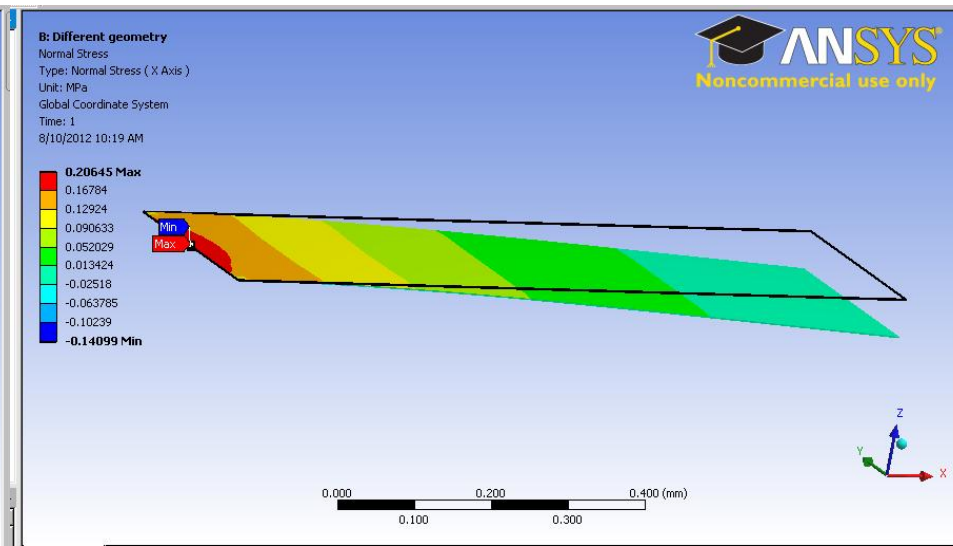
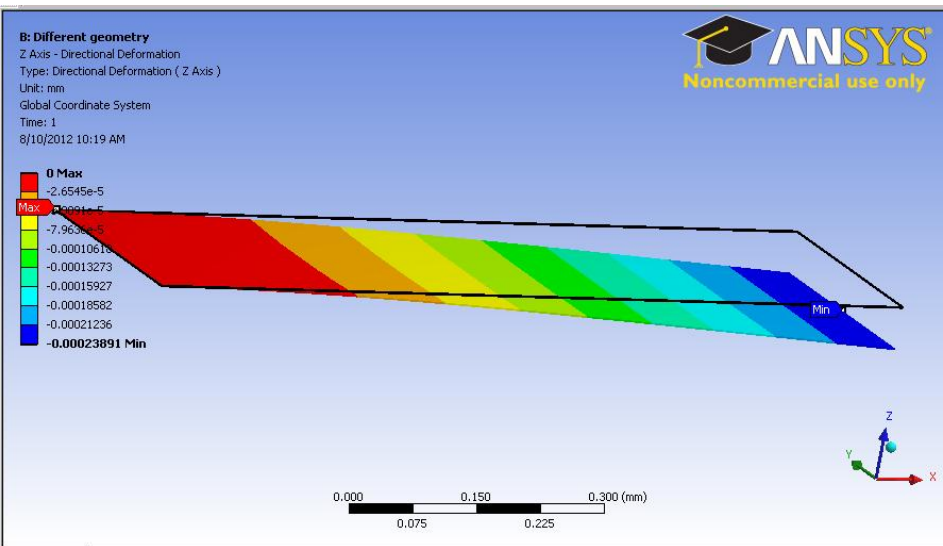
Upper size of the square nodes (μm)	Amount of nodes	Directional deformation (μm)	Maximum stress in X direction (Mpa)	Minimum stress in X direction (Mpa)
16	29572	2.38E-01	0.2063	0.141
17	27001	2.39E-01	0.2063	0.14095
18	24113	2.39E-01	0.20621	0.14087
19	21387	2.39E-01	0.20631	0.14092
20	20193	2.39E-01	0.20645	0.141
21	18081	2.39E-01	0.20629	0.14088
22	15733	2.38E-01	0.20598	0.14064



Results obtained with the numerical model

Results obtained with the numerical model

❖ Deformation and stresses:

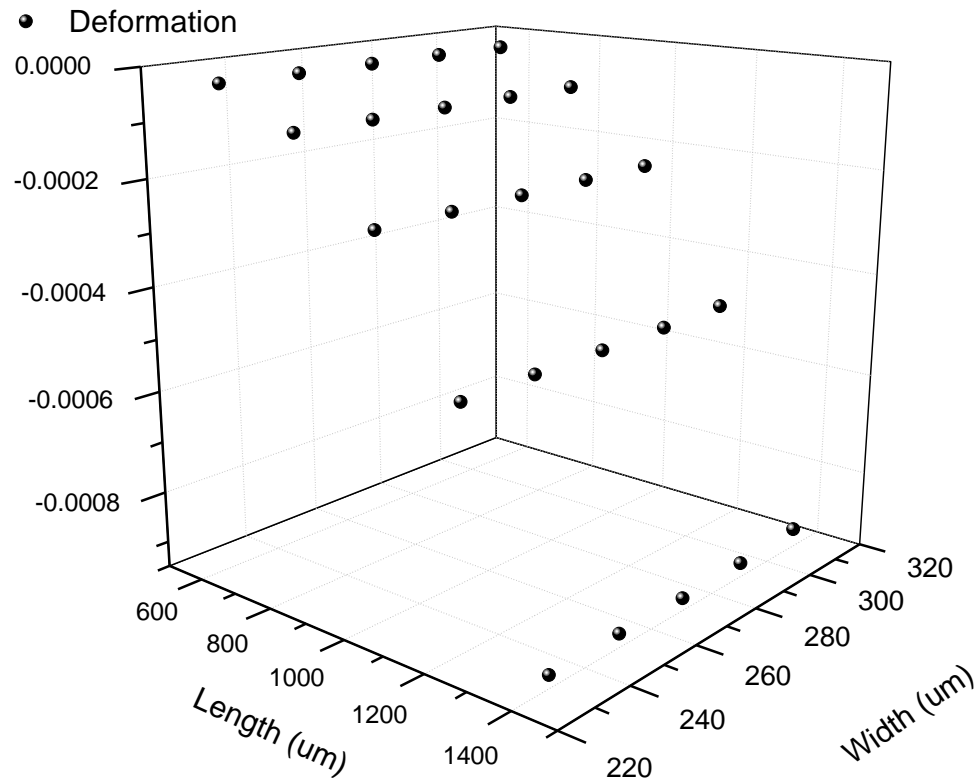


Results obtained with the numerical model

- ❖ As explained before different lengths and widths were used and the deformation and stresses were calculated:
 - Lengths varied from 600 to 1400 μm .
 - Widths varied from 230 to 310 μm .

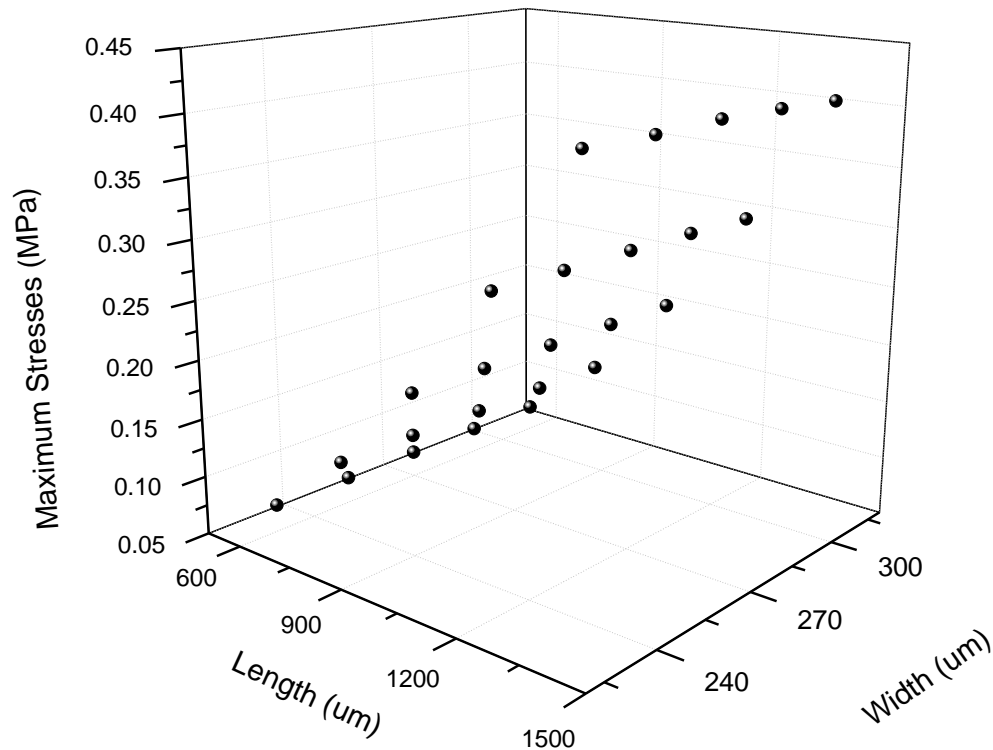
Results obtained with the numerical model

❖ Deformation obtained for different geometries:



Results obtained with the numerical model

❖ Stresses obtained for different geometries:



Results obtained with the numerical model

❖ Future work:

- Develop a shell model to validate the results obtained.



Conclusions and summary

Conclusions and summary

- ❖ The working mechanism and applications of piezoelectric cantilevers was explained.
- ❖ The fabrication processes was summarized in order to know the real applied loads.

Conclusions and summary

- ❖ A model of the cantilever designed by Kobayashi et.al. [5] was made and the meshing was verified.
- ❖ Approximations made:
 - Applied loads.
 - Materials used.
 - Geometry (width and Ti layer).

Conclusions and summary

- ❖ A design criterion to change the resonance frequency was developed:
 - The width doesn't have a significant influence in the internal stresses or the deformation.
 - The internal stresses and the deformations increase when the length increase.

References

- [1]: **Sensors and Actuators, A92 (2001) 156-160.**
- [2]: **Sensors and Actuators, A72 (1999) 179-188.**
- [3]: **Applied Physics Letters, V84 N16 (2004) 3187-3189.**
- [4]: **Meas. Sci. Technol. 17 (2006) R175-R195.**
- [5]: **Thin Solid Films 516 (2008) 5272-5276.**
- [6]: **Sensors and Actuators A117 (2005) 1-7**
- [7]: **IEEE Transactions on electron devices, Vol. ED25, No. 10, Oct 1978, p. 1249.**
- [8]: **Platinum Metals Rev., 2001, 45, (2), 74-82.**
- [9]: **A. Yamada, Journal of power Sources 119-121 (2003) 232-238.**
- [10]: **Mat. Res. Soc. Symp. Proc. Vol. 687, 2002 Materials Research Society.**



Thank You!